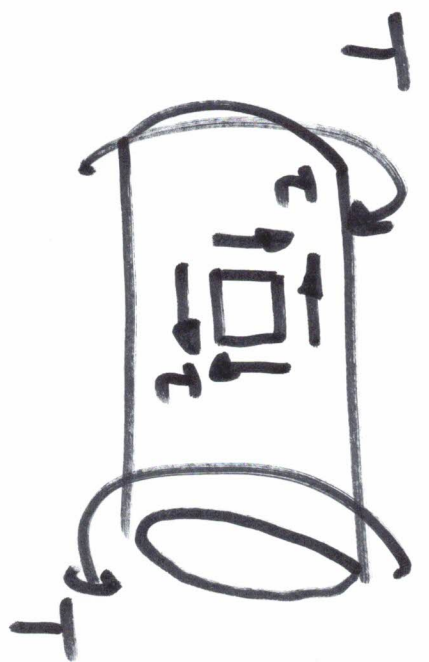
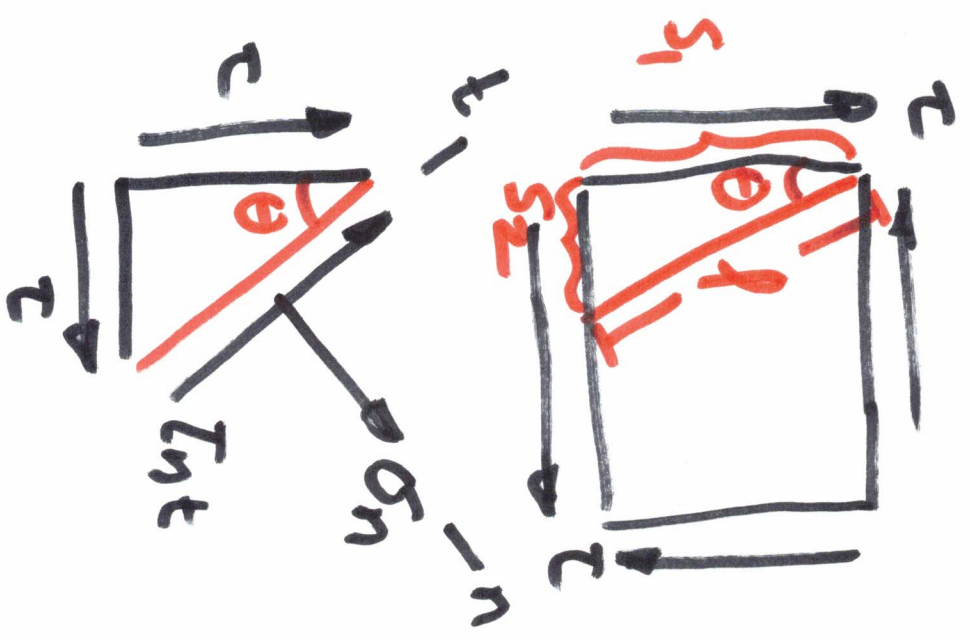


F. Stress State from Torsion

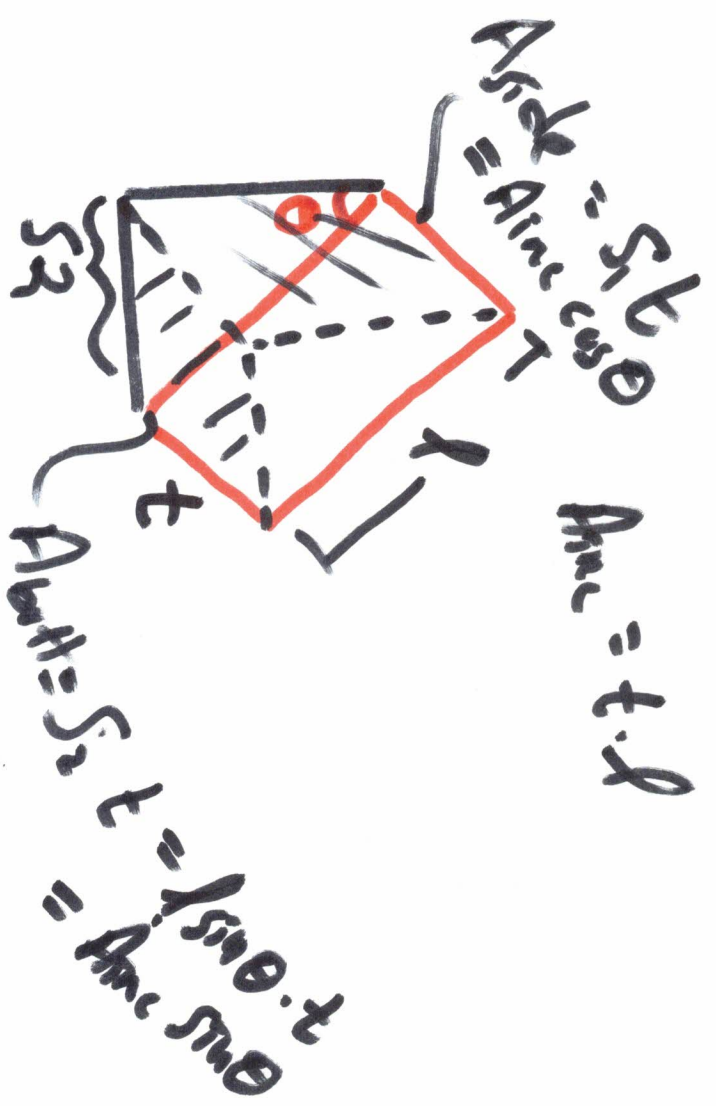


on outside of bar

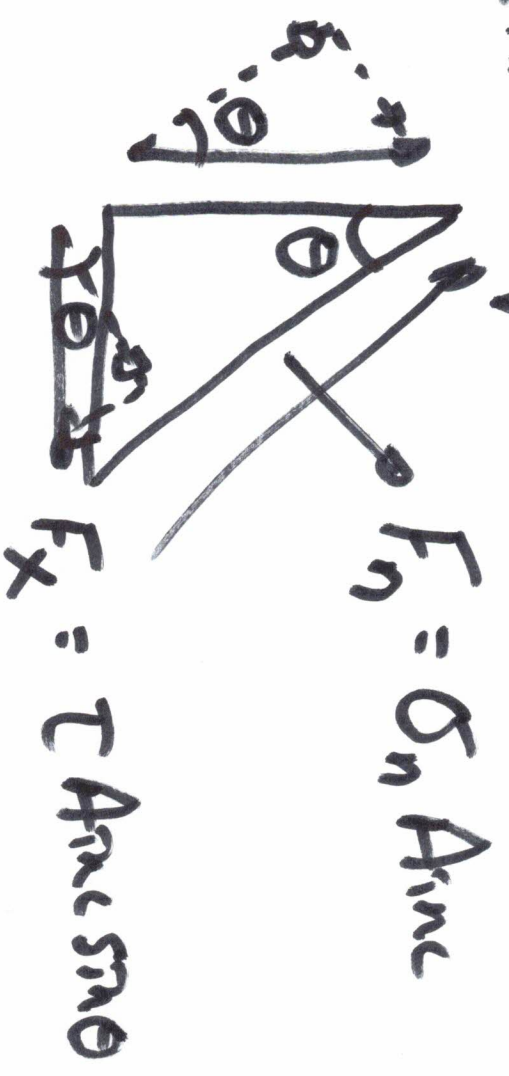
$$\tau = \frac{T \cdot \rho}{I_p}$$



$$\cos \theta = \frac{\sigma_1}{\rho} \quad \sin \theta = \frac{\sigma_2}{\rho}$$



$$F_y = T A_m \cos \theta \quad V = T_{nt} A_m$$

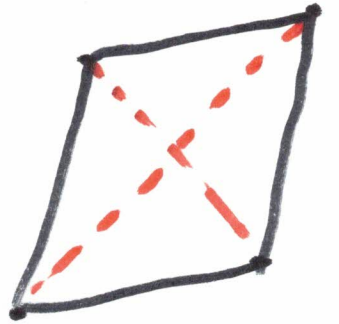
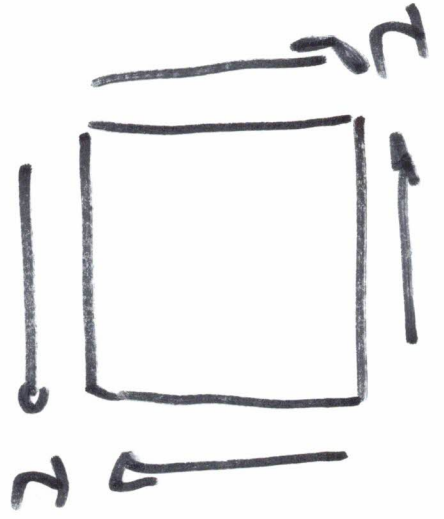
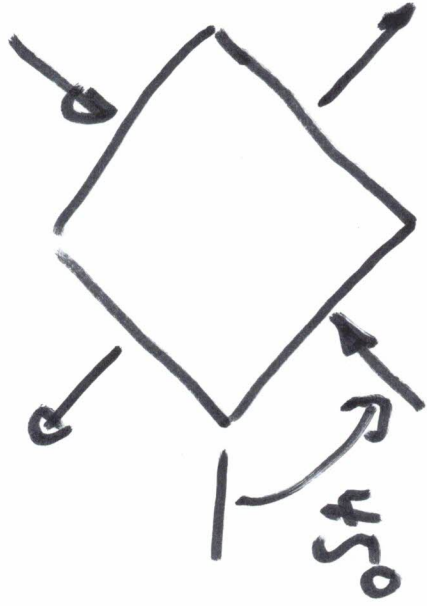
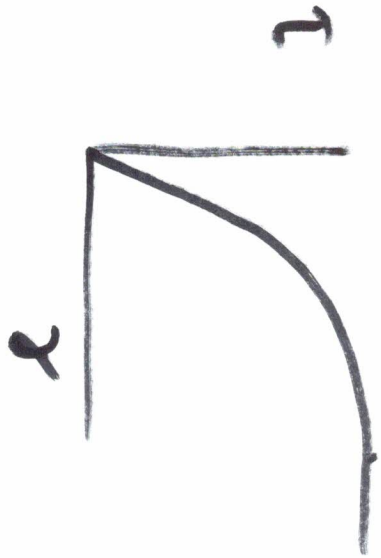


$$\sum F_n \rightarrow + \quad \sigma_n A_m + T A_m \cos \theta \sin \theta + T A_m \sin \theta \cos \theta = 0$$

$$\sum F_x \rightarrow + \quad T_{nt} A_m + (T A_m \cos \theta) \cos \theta - (T A_m \sin \theta) \sin \theta = 0$$

$$\sigma_n = -2 T A_m \sin \theta \cos \theta = \underline{\underline{-T \sin 2\theta}}$$

$$T_{nt} = -T \cos^2 \theta + T \sin^2 \theta = \underline{\underline{-T \cos 2\theta}}$$



Material behavior

- ductile materials tend to fail due to shear stresses (τ)
- brittle materials tend to fail due to normal stresses (σ)

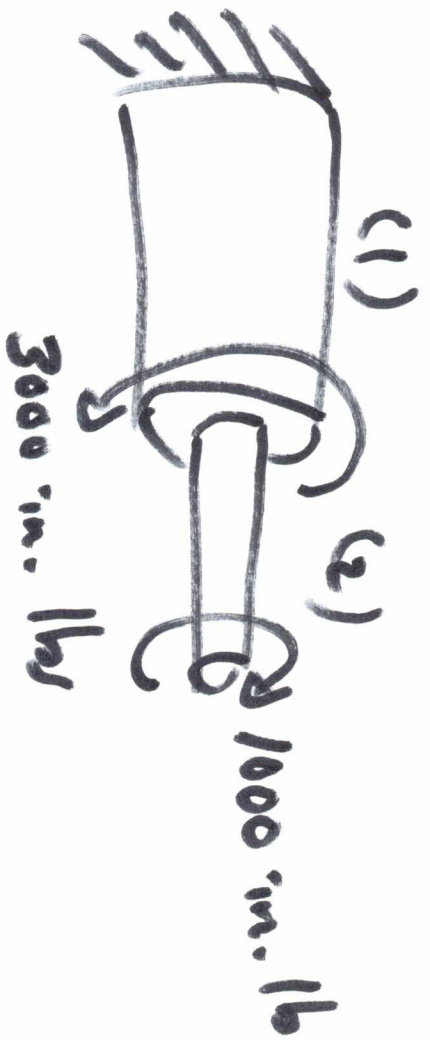
G. Torsion of shafts

$$\phi = \int_0^L \frac{T}{I_p G} dx = \frac{T}{I_p G} \int_0^L dx$$

$$\left[\phi = \frac{TL}{I_p G} \right] \text{ if } T, G, I_p \text{ are constant}$$

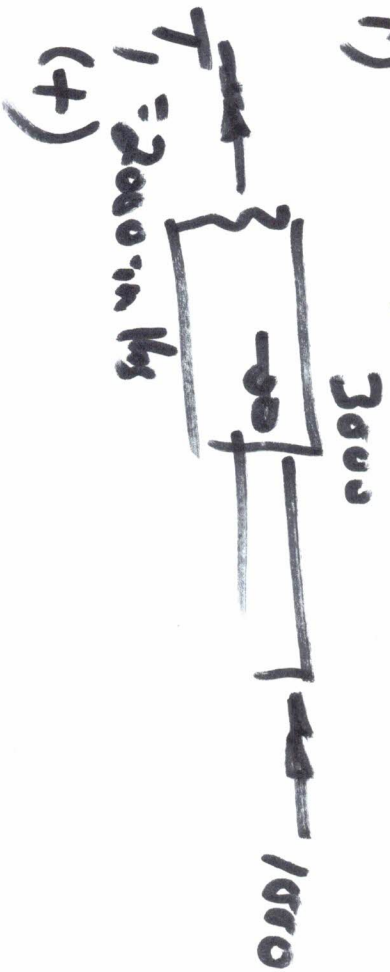
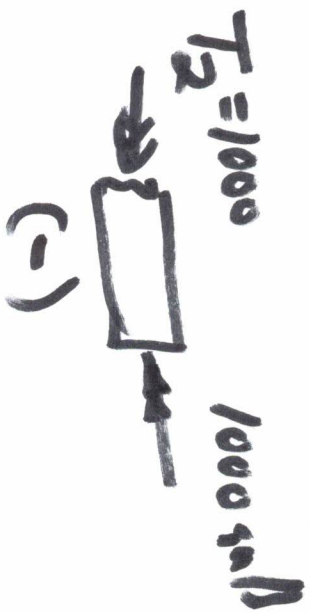
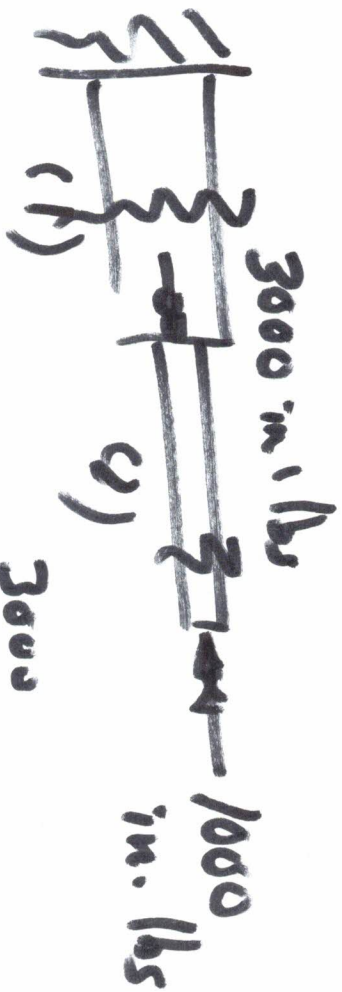
(RADIAN)

$$e = \frac{FL}{AE}$$



$$\phi_{end} = \phi_1 + \phi_2$$

$$\phi_{end} = \frac{T_1 L_1}{E P_1 G} + \frac{T_2 L_2}{E P_2 G}$$



$$\phi_{end} = \frac{2000 L_1}{I_{P1} G_1} - \frac{1000 (L_2)}{I_{P2} G_2}$$

$$T_{max1} = \frac{T_1 d_1/2}{I_{P1}} = \frac{2000 d_1/2}{\pi/32 d_1^4}$$

$$T_{max2} = \frac{1000 d_2/2}{\pi/32 d_2^4}$$